



**SCADA Pro™ 17**  
Structural Analysis & Design

# SCADA Pro - WHAT'S NEW 2017



**Note**

ACE-HELLAS in the context of developing and optimizing its products, and in particular SCADA Pro, has created the new SCADA Pro 2017 with new enhanced capabilities.

Version SCADA Pro17  
May 2017

### What's NEW in SCADA Pro 17?

1. New way of calculating beam reinforcement. Reinforcing with common bars of a specific length.
2. More combinations for the slab's design.
3. New storage capability of dimensioning parameters.
4. Slabs Deflection Control according EC2.
5. Red mark on slab symbol when thickness is less than permitted by regulation
6. Members diagrams, nodes displacements, plate element internal forces, slab strip diagrams view.
7. New possibility of color display of intensive sizes on linear and surface elements, based on the sign.
8. New display capability of the deformation values based on the color gradation
9. Textile Reinforced Mortar(TRM) (ACI549.4R-13 and Triantafillou & Antonopoulos methods).
10. Load bearing masonry check based on Stress Failure Criterion.
11. Rehabilitation are enriched method of beams and columns, using EM4C and Sika materials.
12. 3D DXF-DWG import. Automatic attribution of the cross sections on the drawing lines. Lines and arcs identification.
13. Member Correspondence, to assign the calculated wind and snow loads.
14. New ability to check steel members at shorter times.
15. New command group for merging steel elements.
16. A new warning symbol for inefficiency of the anchoring length in the beams.
17. New command to merge the nodes.
18. New, supervisory and comprehensive print out of the results of buckling and deformation checks (total and per member) of steel structures.
19. Recognition of arcs from dwg 2D-3D.
20. SCADA connection with REVIT via ifc.
21. Import of beams detailing in Drawings without needing to open them in editor.

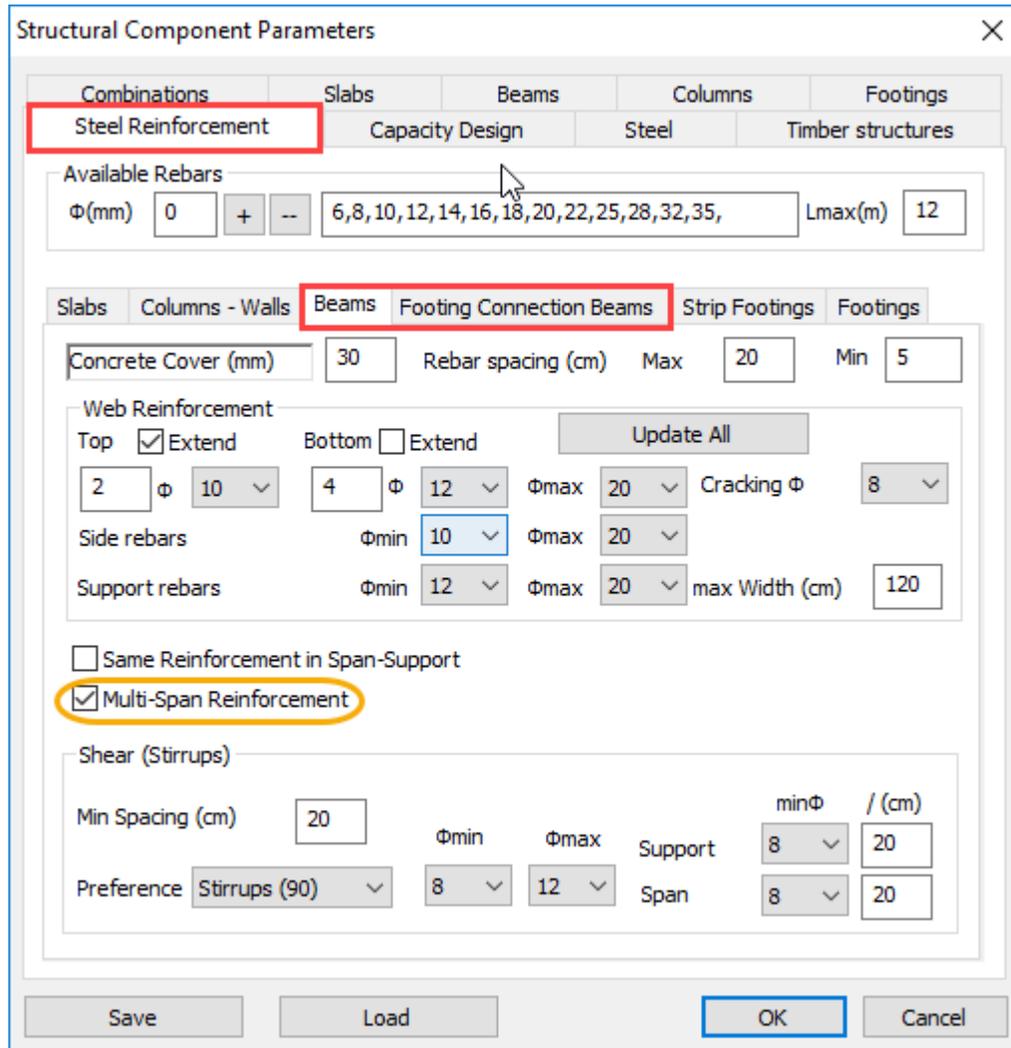
22. Create separate files with support reactions (\* .rea inside scenarios' folder) and two new files in the anal folder: combdispl.txt and combforce.txt. The first contains movements, rotations from combinations, and the second the corresponding intensive forces.
23. New type of design scenario including the EC2 provisions but not the EC8 provisions. In this scenario, the columns' stirrups do not continue in the node.
24. Jacketing for circular cross section.
25. The uniform height distribution of the earthquake in the Eurocode 8 scenario is added.
26. More distinct Attribute points of beams and posts (larger and red).

#### The NEW ADD-ONS of SCADA Pro 17

27. SCADA Pro OCP.
28. Modeling and dimensioning of flat slabs.
29. Punching shear checks.

### What's NEW in SCADA Pro 17?

#### 1. New way of calculating beam reinforcement. Reinforcing with common bars of a specific length

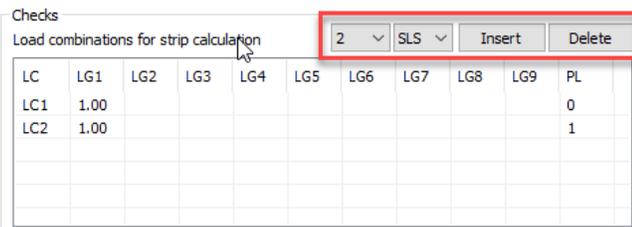
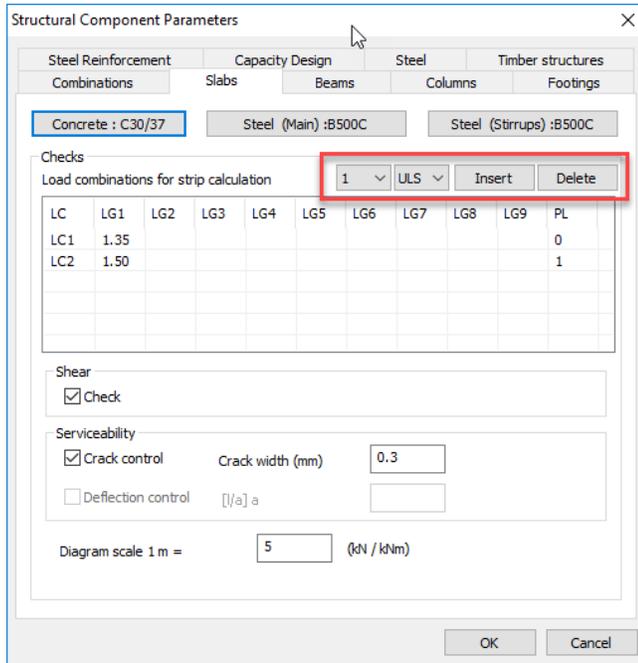


Activate the following checkbox  Multi-Span Reinforcement so that the reinforcement in the openings is common to the entire beam.

The program, taking into account the reinforcement requirements across the beam (supports and openings), places a common bar aimed at the most economical solution.

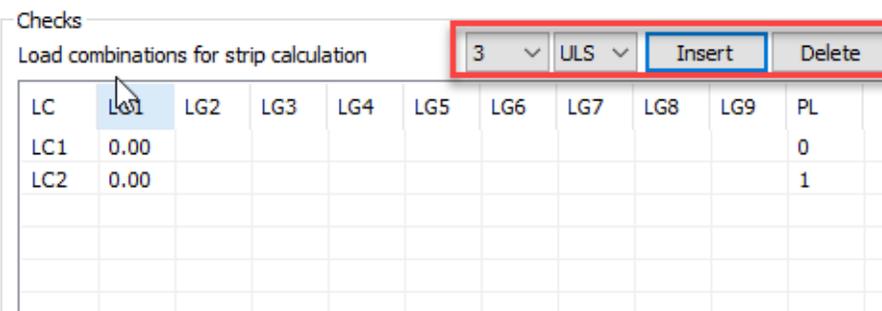
## 2. More combinations for the slab's design

In the new version of Scada Pro there is the feature of introducing more combinations for the slab's design. In the design parameters window, inside Slabs Tab:



There are 2 default combinations, one for the Ultimate and one for the Serviceability Limit States.

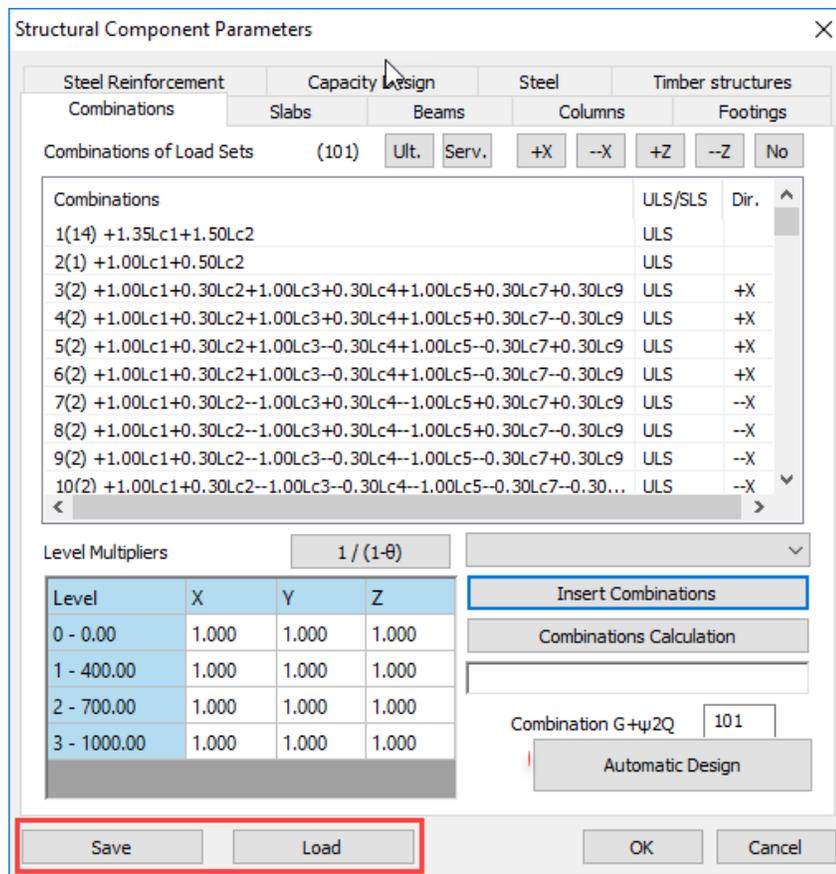
To create a new combination, press, "Insert". The new combination is the combination number 3 and the coefficients are all 0.



Change the coefficients and select the Limit State.  
 Same way to define as much combinations you like, or to modify the ones you already create. The program will use the combination with the worst moment regarding the USL combinations and correspondingly will make deformations checks by the functionality combinations. Using "Delete" button you can delete the created combinations. Only 1 & 2 default combinations cannot be deleted.

### 3. New storage capability of dimensioning parameters

The parameters dialog box in the new Scada Pro version contains two more commands for saving and reading the design parameters of the active scenario.



Once you configure the dimensioning parameters, you can now save them to a file in order to use them in your next projects.

Press "Save" and type a name.

Use "Load" command to apply the parameters already saved.

**⚠ ATTENTION**

A precondition for loading a parameter file is that the current design scenario is the same as the scenario of the parameters. Otherwise you will see the warning message.

**4. Slabs Deflection Control according EC2.**

In the newest SCADA Pro version contains also the slabs **Deflection Control**.

Deflection control based on 7.4.2 and 7.4.3 of EC2 is presented at the end of the results of each slab.

The results of the two checks are shown separately.

```

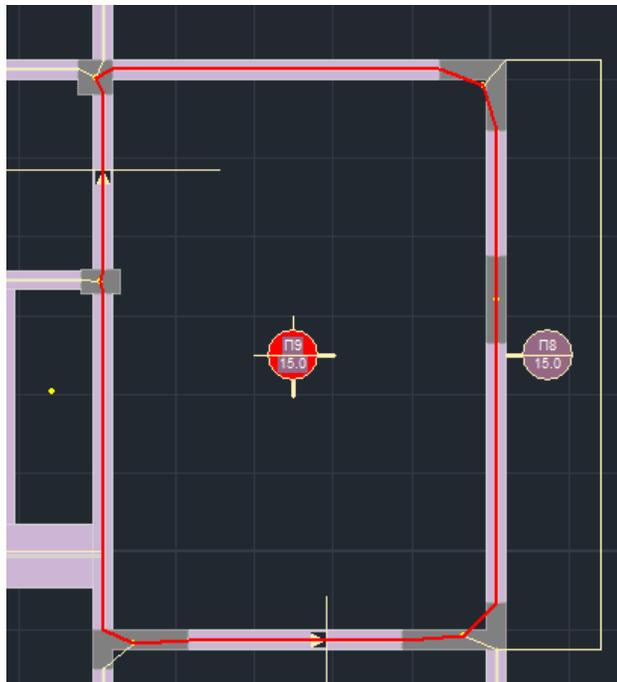
+-----DEFLECTION CONTROL (EC2 7.4.2 & 7.4.3)-----+
| 1/d | 1/d |Suf.|Suggested.min| |Max. M | dul | a |1/a (perm.)|Suf.|
| | perm. | |thick. hs (mm)| | (kNm) | (mm) | | (mm) | |
+-----+-----+-----+-----+-----+-----+-----+
| 34.59| 80.10|YES | 77 | | -7.64| 0.42 | 250 | 18.40 ||YES |
+-----+-----+-----+-----+-----+-----+-----+
    
```

From the first check results a minimum recommended thickness, that can not be proposed for the initial slab recognition, because its reinforcement is required to calculate it.

**⚠ Note:**

The calculation of the sizes of the first check does not involve intensive forces, while the second check considers the serviceability combination (s).

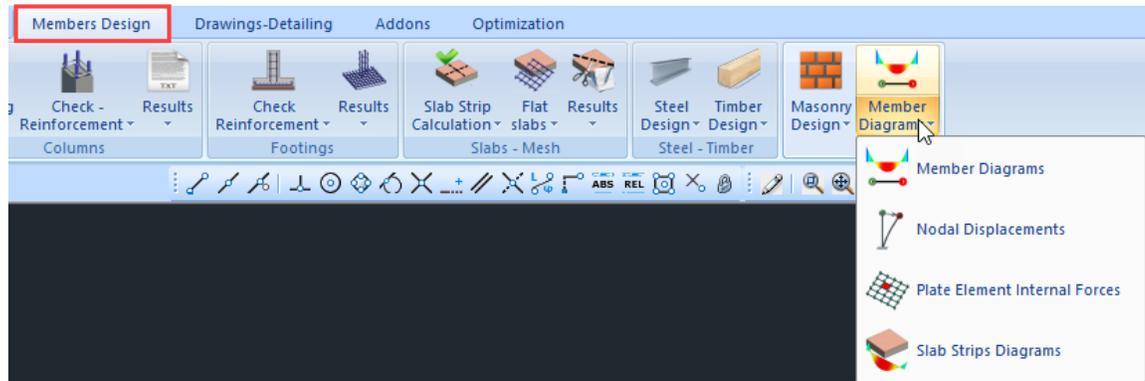
**5. Red mark on slab symbol when thickness is less than permitted by regulation**



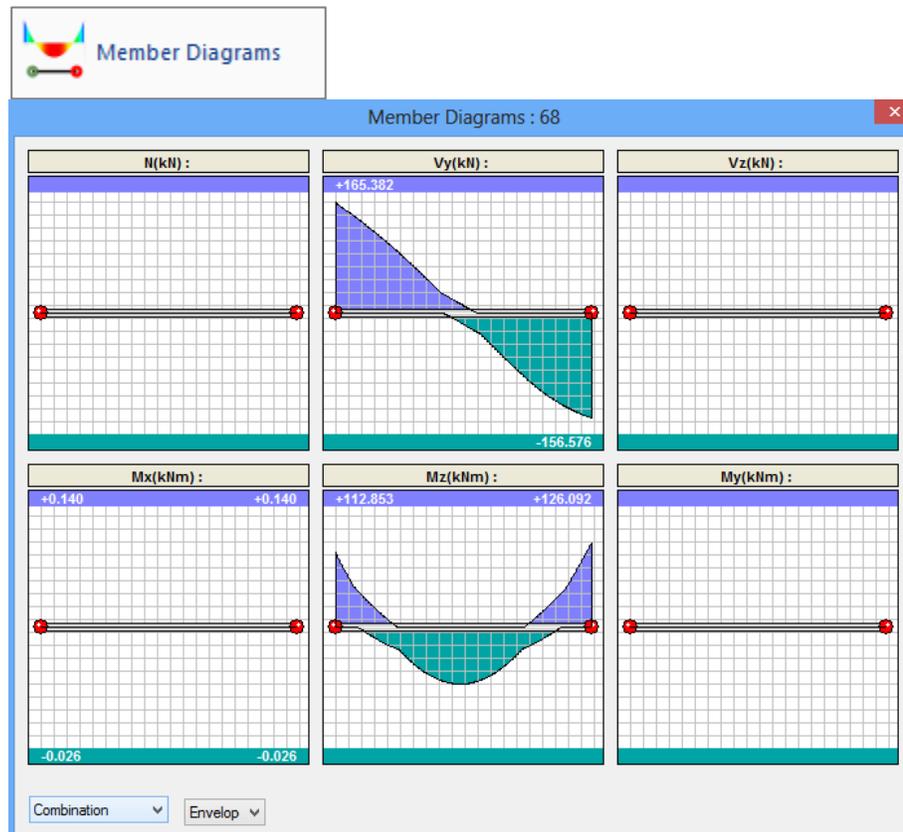
## 6. Members diagrams, nodes displacements, plate element internal forces, slab strip diagrams view

It is now possible to see not only the Members diagrams, but also nodes displacements, plate element internal forces and slab strip diagrams view.

Commands selection can be through Members Design>Members Diagrams



Or with right mouse click on a member.  
Each command opens the respective dialog box:



 Nodal Displacements

Displacements of Node : 34 ✕

Coordinates : 1366.83,1000.00,450.99

Dx(mm)	0.2681
Dy(mm)	-1.2344
Dz(mm)	0.1889
Rx(rad)	0.0000
Ry(rad)	0.0000
Rz(rad)	0.0001

Load Case  ✕

Maximum Rates Exit

 Plate Element Internal Forces

Plate Elements Internal Forces : 53 ✕

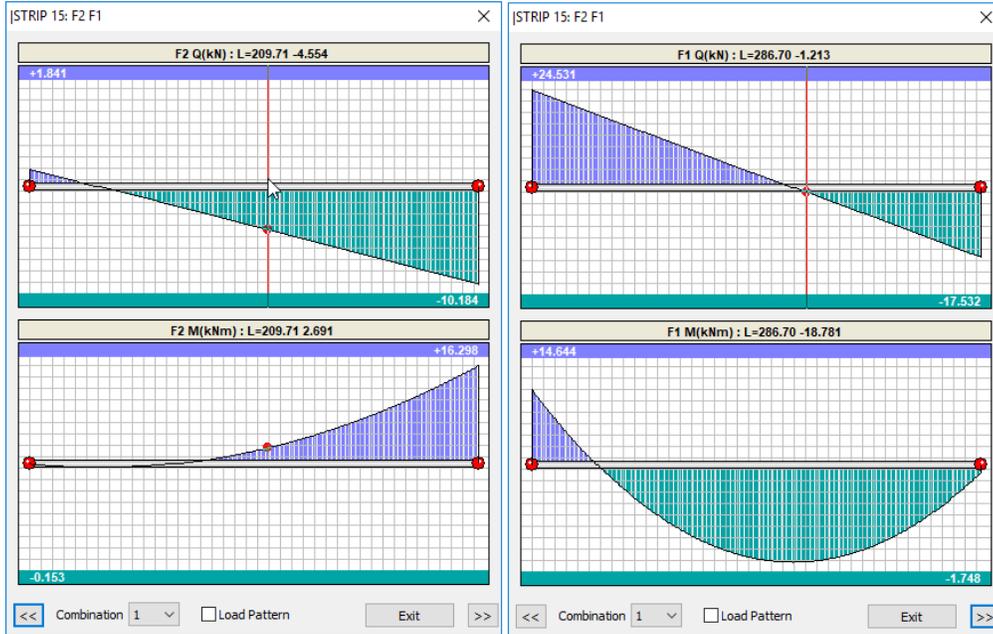
Nodes : 997 , 1027 , 995 , 966

$\sigma_{XX}$ (kN/m <sup>2</sup> )	2476.0000
$\sigma_{YY}$ (kN/m <sup>2</sup> )	-3654.0938
$\sigma_{XY}$ (kN/m <sup>2</sup> )	212.5625
MXX(kNm/m)	193.9150
MYY(kNm/m)	-19.8182
MXY(kNm/m)	-0.9999

Load Case  ✕

Maximum Rates Exit

**Slab Strips Diagrams**

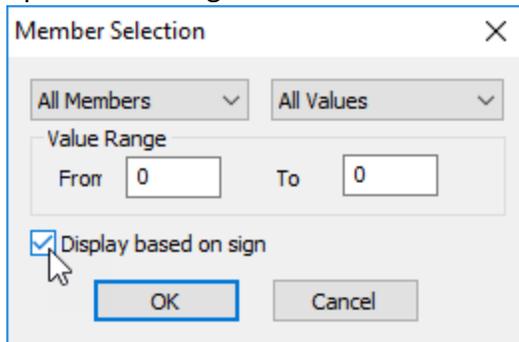


**7. New possibility of color display of intensive sizes on linear and surface elements, based on the sign.**

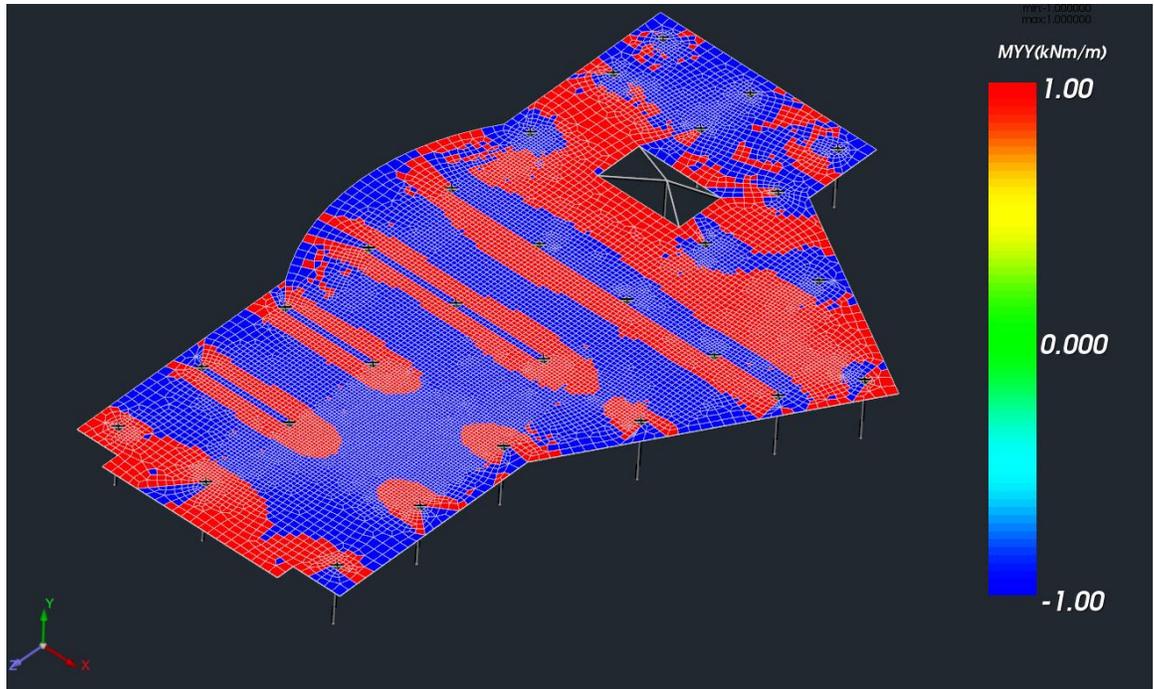
In Post-Processor > Diagrams-Stress Contours dialog box, the “??” command



opens the dialog box:

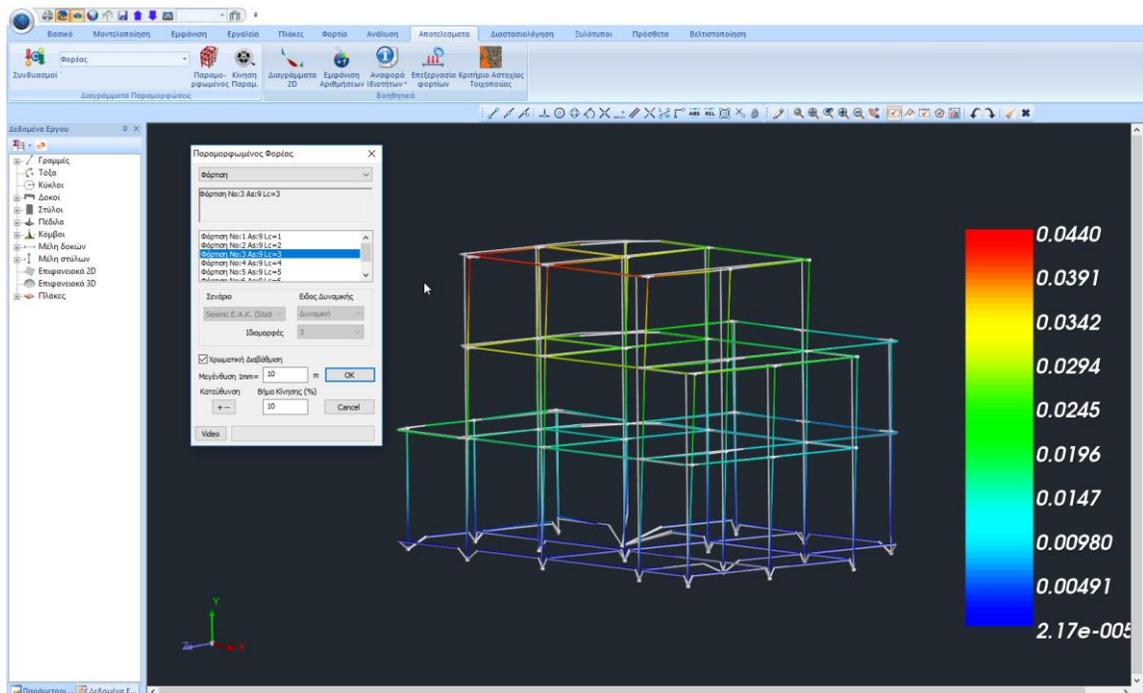


There is now the "Display based on sign" new option. Activating the checkbox, the selected size values display with two different colors, one for the positive values and one for the negative.

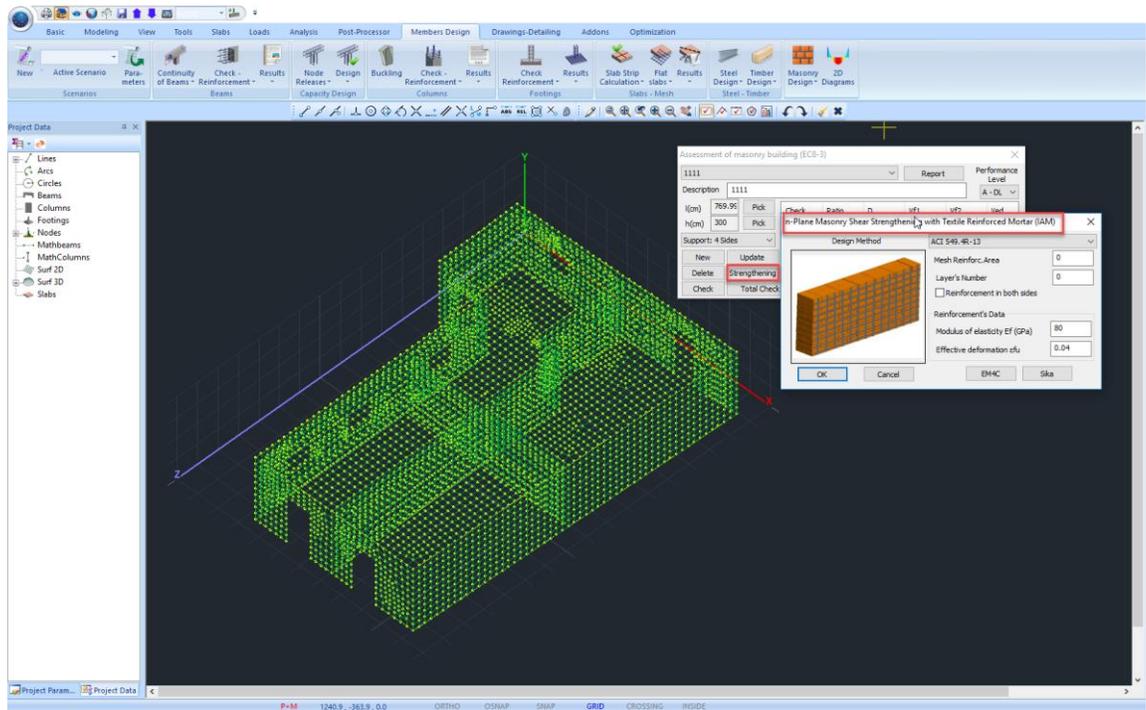


⚠ This option works for all sizes and elements (linear and surface)

### 8. New display capability of the deformation values based on the color gradation



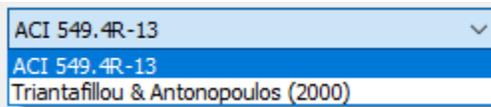
## 9. Textile Reinforced Mortar(TRM) (ACI549.4R-13 and Triantafillou & Antonopoulos methods).



Use Textile Reinforced Mortar for shear reinforcement in plane, defined by the corresponding window for the selected wall from the list.

Select the “Design Method”.

To SCADA Pro contains 2 methods and you can select between

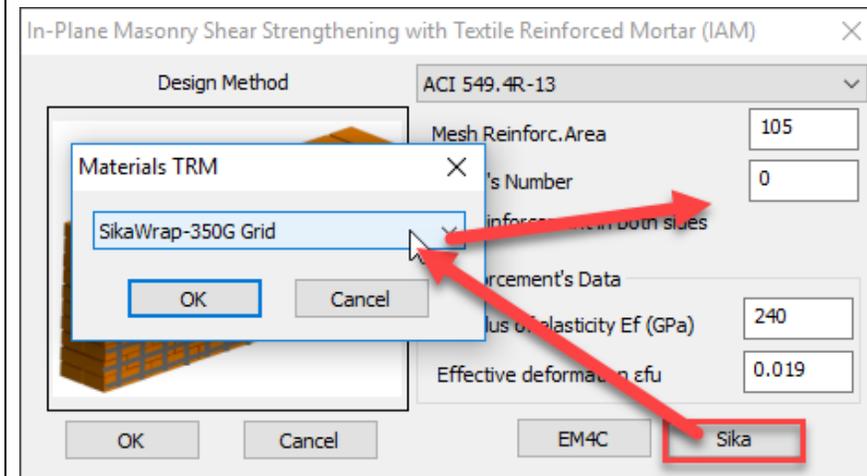
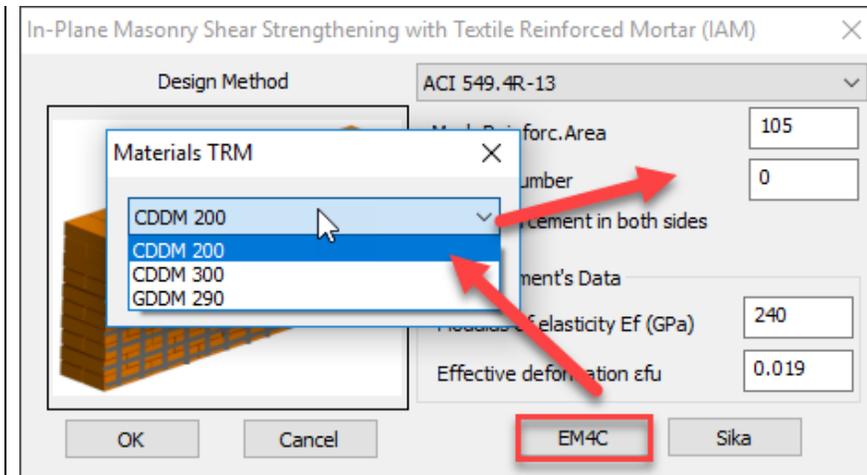


Specify the characteristics of the mesh, based on catalogs and commercial materials.

⚠ In SCADA Pro company materials have been introduced



By selecting the company and the corresponding material the mesh features are automatically filled in by the program.

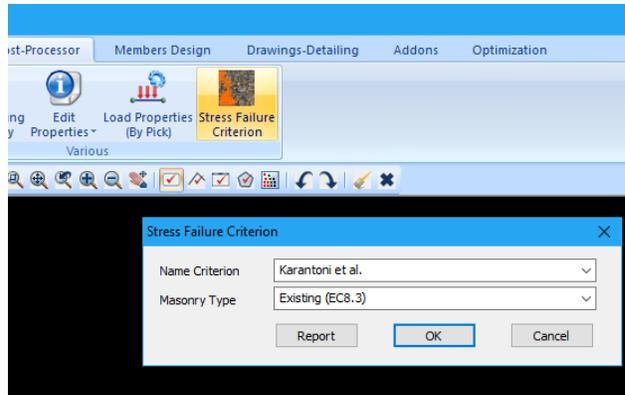


### 10. Load bearing masonry check based on Stress Failure Criterion

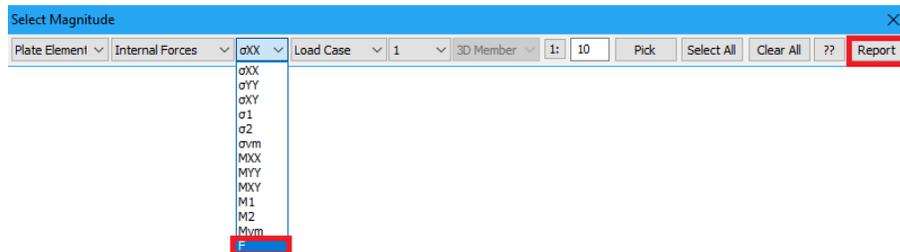
In the new version of SCADA Pro the check of load bearing masonry in terms of stresses based on the Karantoni et al. stress failure criterion is added. The check in terms of stresses is performed in both curved and planar walls for existing or new masonry.

The check command is located in the **Post-Processor** tab where:

- Initially the masonry type is selected (Existing/New).

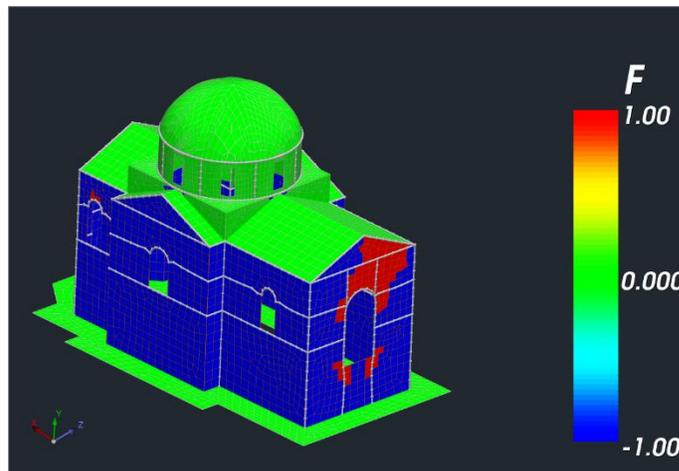


- In the following, from the surface elements stresses bar the F entity is selected.



The model is colored according to the value of the criterion:

- BLUE for sufficiency
- RED for insufficiency
- GREEN for members of different material



For better evaluation of the check results two additional options exist:

- The values of F are written in a txt file for all the surface elements through the Report command.

Name	Comb.	F
***** Plegma - S30 *****		
696	4	-0.549
697	4	-0.573
698	4	-0.625
699	4	-0.731
700	4	-0.798
701	4	-0.807
702	4	-0.761
703	4	-0.748
704	4	-0.679
705	4	-0.333
706	4	-0.519
707	4	-0.338

- A detailed report for every mesh is created.

**Stress Failure Criterion**

**Name of Criterion** Karantoni et al.  
**Masonry Type** Existing (EC8.3)  
**Criterion Description**  $F = \alpha J_2 / f_w^2 + \lambda J_2^{(1/2)} / f_w + \beta I_1 / f_w - 1$   
 SUFFICIENCY :  $\Gamma \alpha F < 0$   
 INSUFFICIENCY :  $\Gamma \alpha F \geq 0$



**Mesh Check**

**Mesh Name :** Plegma S21 **Material :** Masonry stone wall - M2 50 cm  
 Compressive strength  $f_w = 0.000$  (N/mm<sup>2</sup>)  $\gamma_M = 2.20 / 1.50$   
 Tensile strength  $f_{wt} = 0.000$  (N/mm<sup>2</sup>)  $CF = 1.35$   
 Equal biaxial comp. strength  $f_{wc,b} = 0.000$  (N/mm<sup>2</sup>)  
**Criterion Parameters :**  $\alpha = 0.665$   $b = 1.650$   $c_1 = 13.765$   $\lambda_1 = 0.581$   
 $\beta = 3.835$   $f = 0.085$   $c_2 = 0.959$   $\lambda_2 = 0.995$

Number of elements	Total Area (m <sup>2</sup> )	Number of elements that fail	Total Failure Area (%)	Critical Combination			
				ID.	Number of elements that fail	Total Failure Area (%)	F <sub>max</sub>
128	8.64	0	0.00	37	0	0.00	-0.31

#####

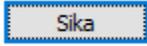
**Mesh Name :** Plegma S22 **Material :** Masonry stone wall - M2 50 cm  
 Compressive strength  $f_w = 0.000$  (N/mm<sup>2</sup>)  $\gamma_M = 2.20 / 1.50$   
 Tensile strength  $f_{wt} = 0.000$  (N/mm<sup>2</sup>)  $CF = 1.35$   
 Equal biaxial comp. strength  $f_{wc,b} = 0.000$  (N/mm<sup>2</sup>)  
**Criterion Parameters :**  $\alpha = 0.665$   $b = 1.650$   $c_1 = 13.765$   $\lambda_1 = 0.581$   
 $\beta = 3.835$   $f = 0.085$   $c_2 = 0.959$   $\lambda_2 = 0.995$

Number of elements	Total Area (m <sup>2</sup> )	Number of elements that fail	Total Failure Area (%)	Critical Combination			
				ID.	Number of elements that fail	Total Failure Area (%)	F <sub>max</sub>
146	7.13	7	7.75	35	4	4.37	0.44

#####

### 11. Rehabilitation methods of beams and columns are enriched, using EM4C and Sika materials

In SCADA Pro, the techniques and the material considered in each rehabilitation method are enriched with the corresponding material and techniques of the companies' EM4C and Sika. The user has direct access in the library of EM4C and Sika materials by pressing the corresponding button, which appears in the dialog boxes related to column reinforcement.

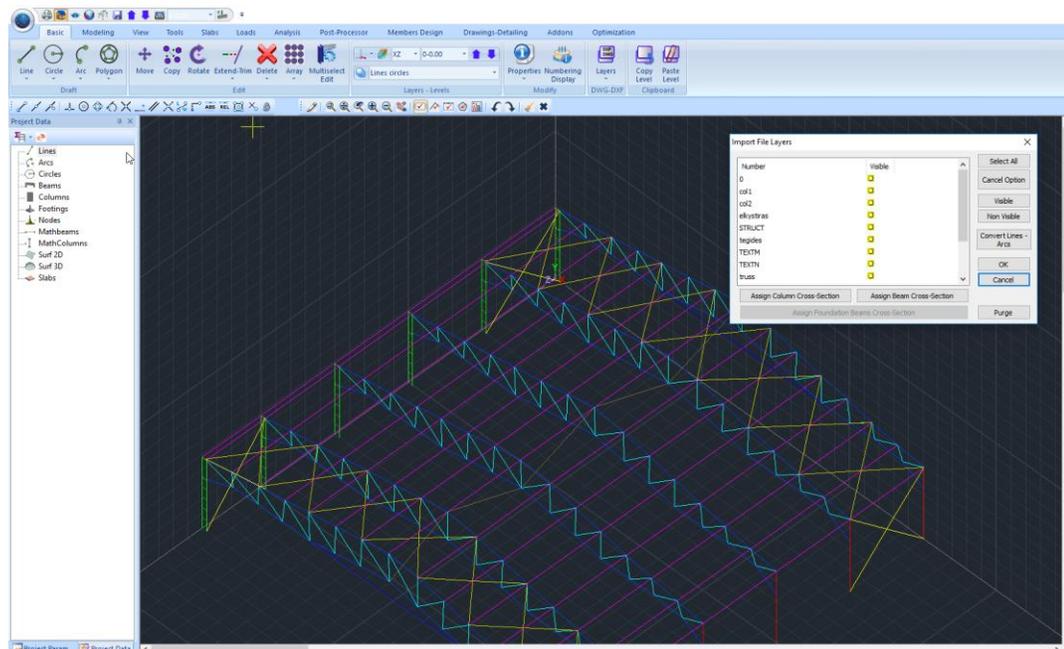
Select one command  , and then select the appropriate material for each rehabilitation method. Also, select the following button  and a PDF file, with an analytical description of the material properties as well as information related to its use, is automatically downloaded.

### 12. 3D DXF-DWG import. Automatic attribution of the cross sections on the drawing lines. Lines and arcs identification.

SCADA Pro17 gives you the opportunity, not only to import a 3D dwg-dxf file, but also to assign automatically the respective sections to the drawing lines.

First select the 3D display of Scada  and through the command Insert, insert the 3D

design. Selecting  opens the list with all project's layers.

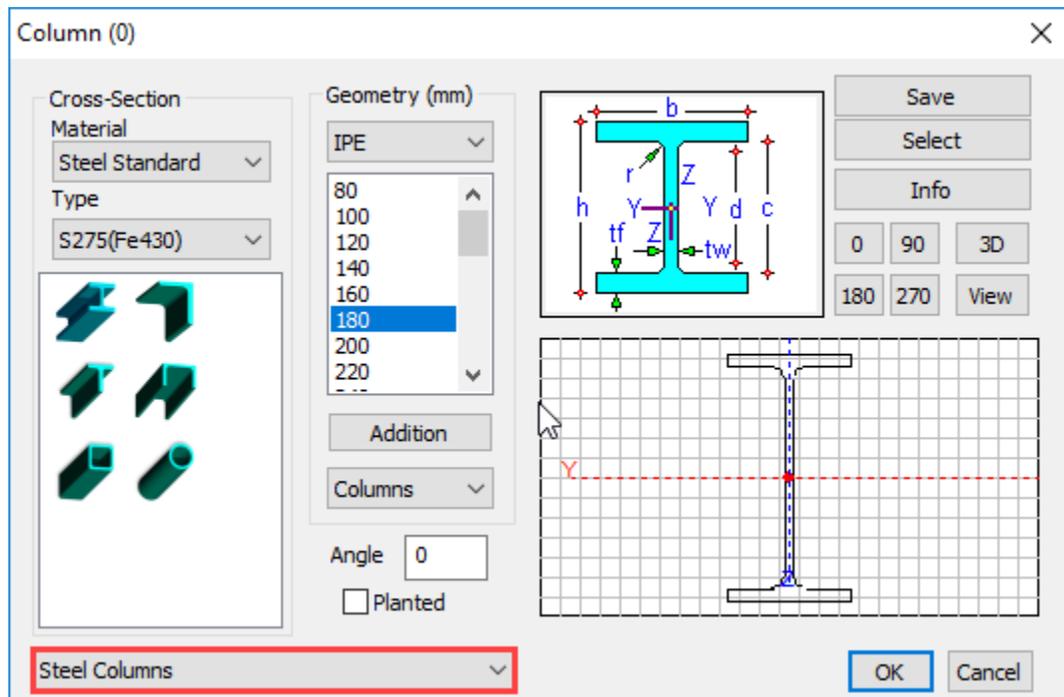


For the automatic attribution of the cross sections on the drawing lines, is necessary the correct matching of the lines in the respective layers.

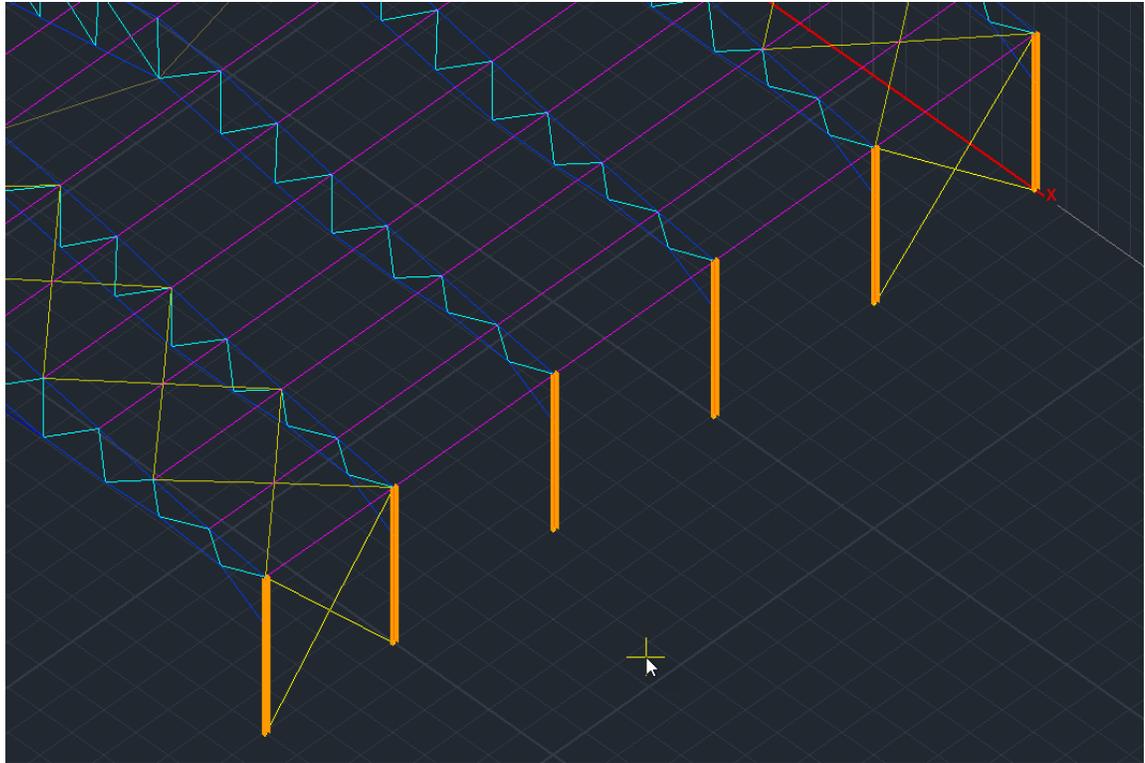
Choose a layer from the list and depending on whether includes columns or beams, select the corresponding command at the bottom of the window



Automatically opens the cross sections window, to select the one that will be assigned on all the lines of the selected layer. Also, choose the angle, the insertion point and the Scada's layer in which they will join.



Members created automatically containing physical and mathematical properties.

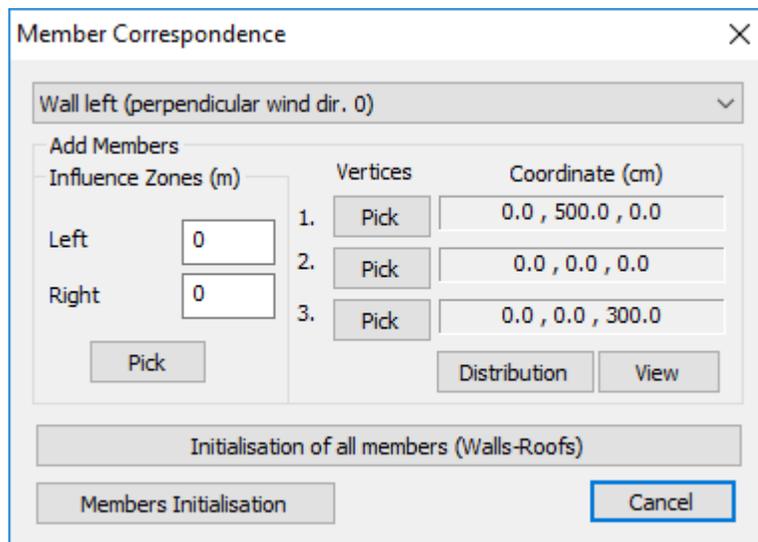


### 13. Member Correspondence, to assign the calculated wind and snow loads

In the new version of SCADA Pro, completed and integrated the automatic calculation of influence zones for linear members in order to make the distribution of wind and snow loads.

**⚠** *Remind that until now the automatic distribution was only for the structures derived from Templates. Now enable this distribution on any surface.*

By selecting the command now opens the following dialog box



The part on the old definition of the influence zones did not change but added to the right a new part to define the area with three points.

The definition always concerns the active area

Wall left (perpendicular wind dir. 0)

*Better to start the procedure by pressing the "Members Initialization" button.*

Indicate the point graphically with the following particularity:

- The first two points define the direction by which the automatic calculation of influence surfaces made for items which are parallel to this direction.  
Note also that the distribution will be for all linear members belonging to this level and are parallel to the first direction.
- After you define the three points, press the "Distribution" button and the program automatically makes the distribution and displays it.

Similarly for the other walls.

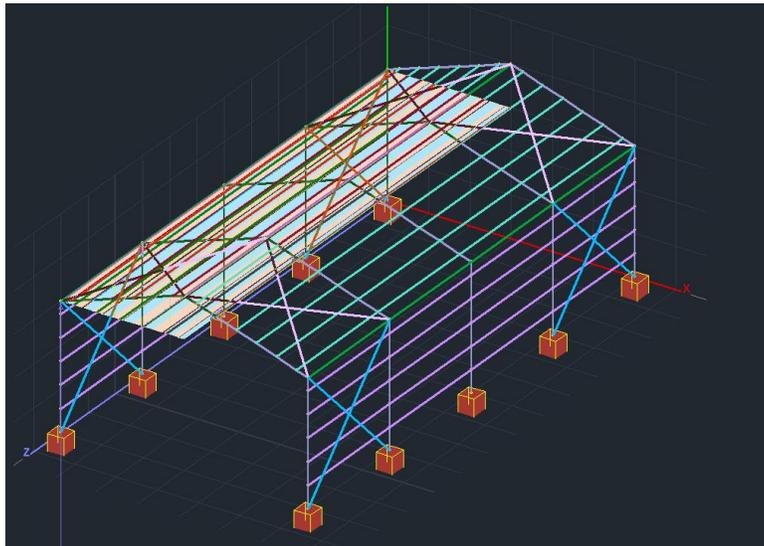
Concerning the roofs, the definition can be sequentially.

First select the roof

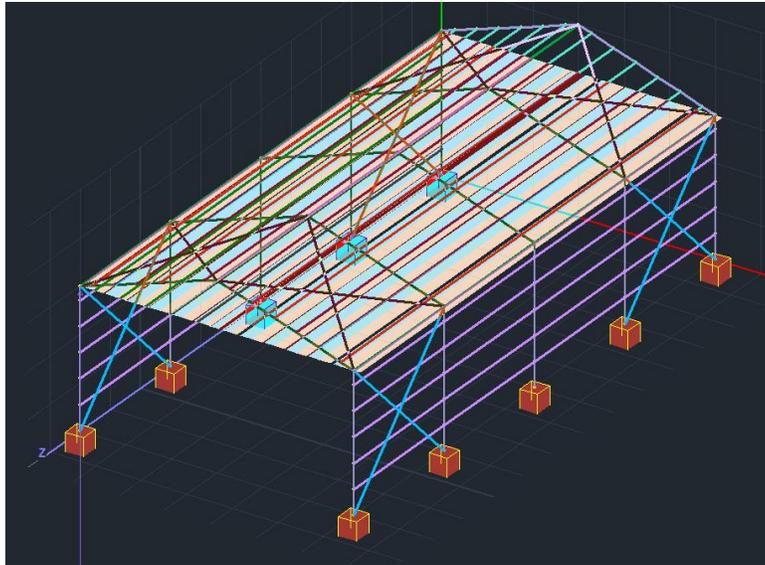
Roof No. 1

, then you must define the individual areas.

First define the left slope indicating graphically the 3 points

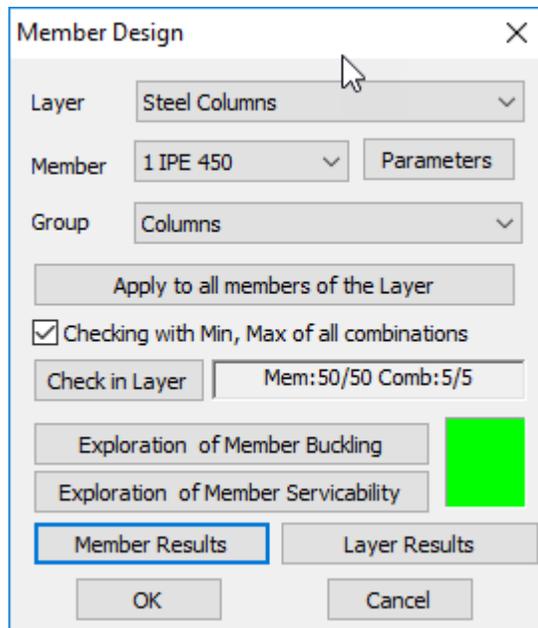


and then the right. The overall result is the following



- ⚠ Finally it is worth noting that if the walls are properly defined there is NO need of more definition. Just select each wall and press «Distribution». The distribution becomes and simultaneously displays on the linear members belonging to this wall.
- ⚠ Same for the flat roofs only.

**14. New ability to check steel members at shorter times.**



Activating the option  Checking with Min, Max of all combinations , in checks will be taking into account only the maximum and minimum values of the intensive forces resulting from all combinations, excluding the intermediate values, so the process will be completed at noticeably shorter times.

### 15. New command group for merging steel elements.

In “Members Design” added a new command group that provides steel elements merging.



Merge elements means that, either automatically or manually, the individual parts of a single element, merge in each buckling direction. Meaning that, the buckling length is considered computationally, not the actual length of the element, but the unified from the beginning to the end of the column or beam, respectively.

In addition, in the presentation of the results, for these merged elements, the worst results display only once and not for each individual part, as it was so far.

Finally, in automatic merging, there is the definition of discontinuity levels, horizontal or vertical, used as merging boundaries of a continuous element.

### 16. New command for member's direction redefinition.

In Tools > Member added a new command named “Direction Redefinition”.



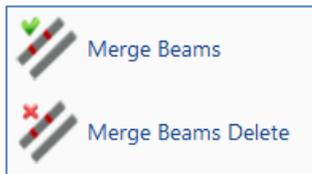
This command should be used when one or both of the following messages appear in the Model Checks Reports:

Error1678: The column 21 has been assigned with wrong orientation  
 There are members with wrong local axis

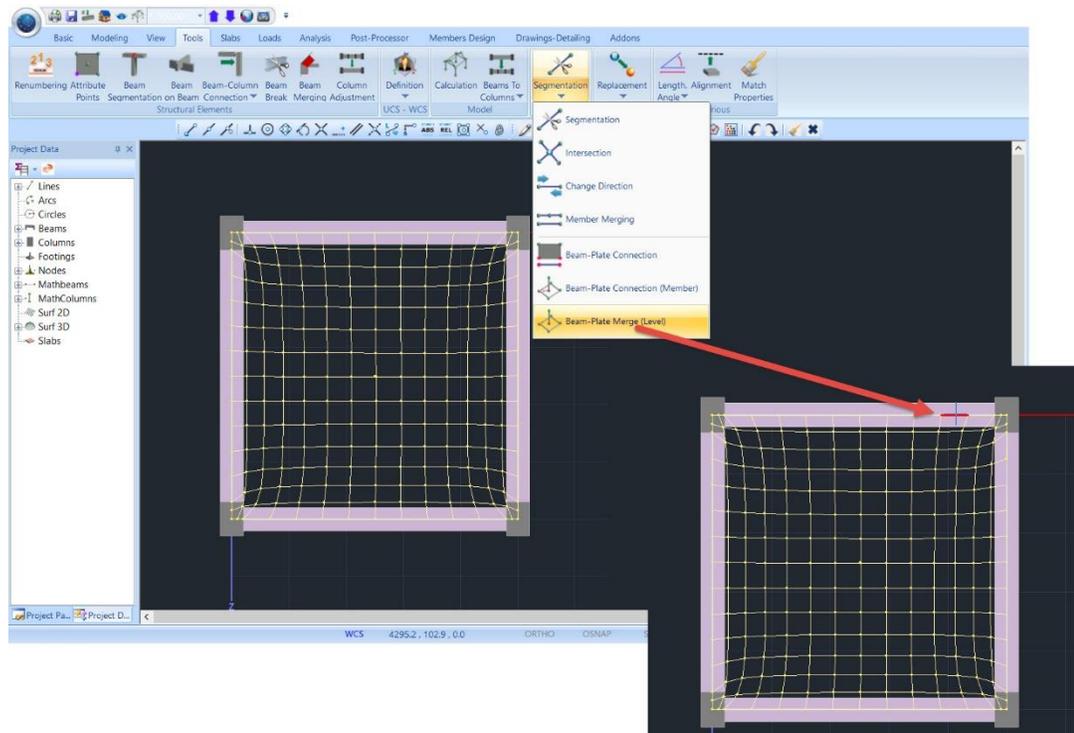
The first one, which concerns only the columns, has to do with the direction of their placement (the correct direction is from the bottom to the top), while the second is a general message concerning beams and columns, and especially for the beams, appears when they are not placed with the program conversion, from left to right and from top to bottom.

So when the above messages appear, using the "Direction Redefinition" command the program corrects automatically the orientation for the entire model.

**17. New command that Merge Beams**



Where the beams include surface elements is a need to break the members of the beams in order to ensure the necessary connections between the linear and surface elements.



Consequently, breaking the beam in small portions creates the need for unification in order to be able to dimensioned as a single member. This is accomplished by using the



command Merge Beams.

Select the command, and then one by one in succession the parts of the beam. Continue with “Continuity of Beams” and “Check Reinforcement”.

If for some reason you wish to delete a preliminary merging, select the command



and then the first element of the unified beam. Right click to complete.

### 18. A new warning symbol for inefficiency of the anchoring length in the beams.

The way of calculating the lbd anchorage lengths for different regulations is summarized below:

The total lbd is calculated and divided into l1 and l2. l1 is the linear anchorage length, and l2 is the one that rotates in the node.

#### NOTES:

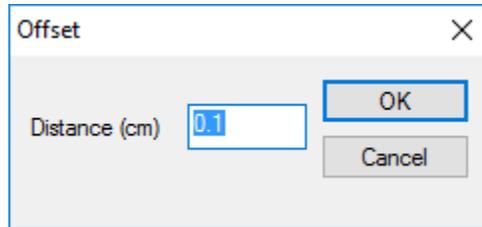
- ⚠ EC2 does not provide for a minimum linear anchorage length but provides for a minimum TOTAL anchorage length ( $l1 + l2$ ) which also calls it  $l_{b, min}$ .
- ⚠ EC8 in paragraph 5.6.2, among others, provides ONLY for DCH the anchorage length to be only linear (excessive).

Based on the above, resulting:

1. For EC2 w/o EC8 scenario as well as for all EC with DCL and DCM ductility classes, it does not obey a minimum linear anchorage length  $l_{b, min}$ , but checks the total length lbd with  $l_{b, min}$  according to 8.4.4 Of the EC2.  
So, there will never be an error message because if the anchorage length is bigger than the width of the support, the bar will reach the face and then turn to the node.
  2. For EC with DCH high ductility class, it obeys the minimum linear anchorage length according to 5.6.2 of EC8 . The error message will be displayed.
- ⚠ In addition, the affinity regions are now taken into account for calculating  $l_b$ . The upper reinforcement is region II while the lower I.

## 19. New command to merge the nodes

### Merge



Command to merge the nodes in small distances between them.

Select the command and specify a distance value. Nodes at a distance less or equal to this will be merged, resulting in a single node.

20. New, supervisory and comprehensive print out of the results of buckling and deformation checks (total and per member) of steel structures

21. Recognition of arcs from dwg 2D-3D

22. SCADA connection with REVIT via ifc

23. Import of beams detailing in Drawings without needing to open them in editor

24. Create separate files with support reactions (\* .rea inside scenarios' folder) and two new files in the anal folder: combdispl.txt and combforce.txt. The first contains movements, rotations from combinations, and the second the corresponding intensive forces.

25. New type of design scenario including the EC2 provisions but not the EC8 provisions. In this scenario, the columns' stirrups do not continue in the node.

26. Jacketing for circular cross section

27. The uniform height distribution of the earthquake in the Eurocode 8 scenario is added

28. More distinct Attribute points of beams and posts (larger and red)

## The NEW ADD-ONS of SCADA Pro 17

### 1. SCADA Pro OCP

SCADA Pro OCP is a new module of SCADA Pro that represents an advanced, real-world, optimum design computing platform for real-world civil engineering structures. The main goal for the implementation of SCADA Pro OCP module is to **reduce construction and material cost** consistent with the required performance, reliability, quality and safety within an innovative technological framework.

SCADA Pro OCP module provide:

- **Advanced** and **easy** to use ribbon-based interface makes structural optimization a **single-click** process allowing numerous customizable options.
- The option of selecting **multiple criteria** related to the cost of the structure such as construction cost, construction of materials, and environmental cost during the life span of the structure. These criteria used either as "Objectives" or as "Constraints", which are taken into account in addition to those imposed by the design code regulations.
- Solve optimization problems by selecting the solution algorithm from a list of **deterministic** and **probabilistic search numerical algorithms** that are at the cutting edge of technology, which can replace the "trial and error" traditional process of structural design and with an optimized solution quickly obtained.
- Πολλαπλές επιλογές για τον καθορισμό του εύρους των **μεταβλητών σχεδιασμού** και την ομαδοποίησή τους είτε σε **επίπεδο διατομής** ή σε **επίπεδο δομικού στοιχείου**.
- Multiple options for determining the value range of the **design variables** and grouping them either **by type of cross-section** or **by type of structural element**.
- **Comparison of the initial design with the optimum one.**

Commands are grouped into sections according to their type of use.

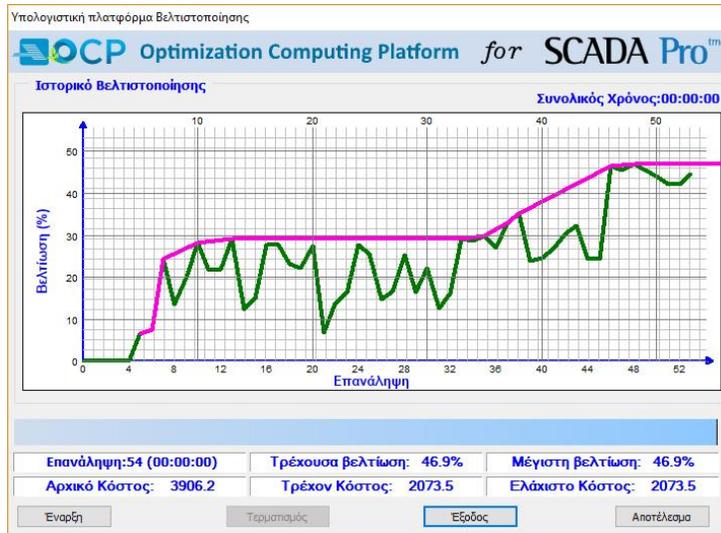


The optimization process is performed in two stages:

- The first stage is the definition of the basic parameters of the project:  
 (a) the optimization criterion (objective function)

- (b) additional constraints in terms of cost or performance apart from the design code checks
- (c) the limits of variation of the cross-sectional dimensions (design bounds) of the structural elements (design variables).

• In the second phase is the definition of the optimization algorithm, the convergence criterion of the iterative solution process and its immediate execution.



After completing the iterative optimization process, it is possible to analyze the results obtained with parallel comparison of the initial parameter values with the optimum values.

Step Number	Failure Degree	Total Cost
1	Max	5461.57
2	Min	2030.09
3	Init	3906.22
4	1.02	4032.28
5	0.00	3649.32
6	0.00	3611.71
7	0.00	2951.76
8	0.00	3380.71
9	0.00	3126.82
10	0.00	2805.49
11	0.00	3054.48
12	0.00	3050.81
13	0.00	2768.42
14	0.00	3422.02
15	0.00	3326.07
16	1.02	2737.10
17	1.02	2763.61

Αναφορά

Εξώφυλλο

Τεχνική Αναφορά

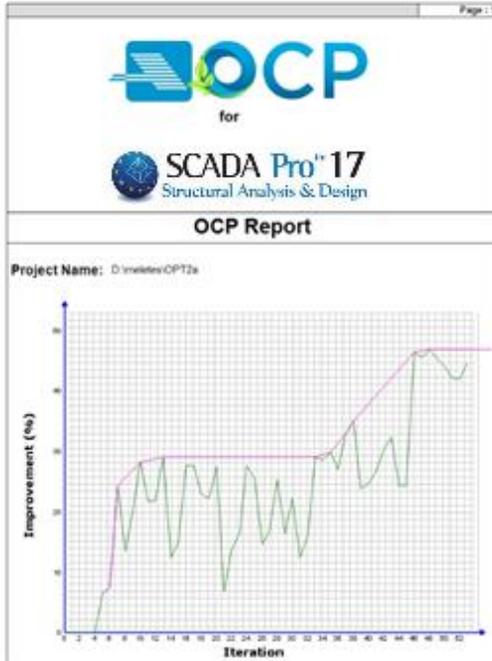
Σύνοψη

Στοιχεία Διατομής

Αναλυτικά Αποτελέσματα

Εμφάνιση Αναφοράς

There is also the option of exporting results, analyzing all the parameters of the optimization problem and the optimization history diagram; the value variation diagram of the optimization criterion (objective function) in each step of the iterative process.



**Technical Report**

The current version of ACE OCP is equipped with three state-of-the-art search algorithms, while two objective criteria to be optimized (either minimized or maximized) are supported. The basic assumptions for the calculation of the two objectives along with a short description of the three algorithms are provided below.

**Objectives**

Material Cost stands for the cost of material quantities used for the construction of the structural system under investigation. For the case of RC structures this cost is calculated as the sum of cost of concrete (volume times concrete unit cost) plus the cost of reinforcement (length of longitudinal and transverse reinforcement times unit cost), while for the case of steel structures this cost is calculated as the sum of the cost for the structural steel weight of steel times unit cost.

Construction Cost stands for the cost of the construction of the structural system under investigation. While in addition to the cost of material the labor cost is also considered. Labor and material costs are completely different entities, with two commonalities. Both types of costs can be deducted and both are used to make a product to customers. Both costs are calculated during the budgetary process and are typically considered when determining the amount to charge for the end product. The labor cost is calculated based on the unit costs given in the productivity tab where the user provides the productivity rates for three groups of elements (Beams, columns and slabs). The productivity rates refer to time required for the construction of unit volume or weight for the concrete, steel reinforcement, construction steel and/or aluminum. The labor cost for each group of elements (Beams, columns and slabs) is calculated as the sum of concrete volume times the corresponding productivity rate plus the reinforcement weight times the corresponding productivity rate plus the weight of the structural steel for this type of elements times the corresponding productivity rate. Then this sum that corresponds to working time (hours) is multiplied by the labor unit cost (currency/h).

**Search Algorithms**

Search Algorithms:  
ACE OCP software is integrated with three algorithms, belonging to two categories: Probabilistic and Deterministic search. In probabilistic search the Differential Evolution (DE) algorithm is available together with a pure Random Search (RS) one that is based on Latin Hypercube Sampling (LHS). In deterministic search the Projected Quasi-Newton (PQN) algorithm is provided.

Random Search (RS) option is suggested for the case of acceptable sampling of the design space for the convergence preferences of the user. Gives an indication on the order of improvement that can be achieved for the problem at hand. RS ensures that all portions of the search space are properly represented into N samples. According to RS the uniform distribution function for each variable is divided into a number of segments of equal marginal probability. These segments are randomly selected for each variable and randomly shuffled among different variables to define the samples. According to RS a sample is constructed by dividing first the range of each of the D variables into N non-overlapping equal segments, and then a sample with dimension D is created by randomly picking the values of all parameters. Thus, the D-space is partitioned into ND segments and a single value is selected randomly from each cell, producing a set of size D. The values from the ND space are randomly matched to create N samples.

Projected Quasi-Newton (PQN) option is suggested for the case of with high complexity in terms of FE model (many degrees of freedom). PQN is a steepest descent algorithm for noisy optimization problems and it is intended for problems with optimization landscapes that look like the image above (i.e. with many local minima). PQN is a hybrid of a projected quasi-Newton or Gauss-Newton algorithm for nonlinear least squares problems and a deterministic global-based search algorithm. The gradients for the quasi-Newton method and the Jacobians for the Gauss-Newton iteration are approximated with finite differences, and the difference increment varies as the optimization progresses. The points on the difference stencil are also used to guide a direct search. PQN is based on a sampling method that controls the progress of the optimization by evaluating (sampling) the objective function at feasible points. Sampling methods do not require gradient information, but may, as PQN does, attempt to infer gradients and even Hessian information from the sampling.

Differential Evolution (DE) option is suggested for the case of problems with high complexity in terms of optimization modeling (many design variables) for exhaustive search. DE is a stochastic population-based evolutionary algorithm for global optimization. DE follows the outline of the evolutionary algorithms with some differences in mutation and selection operators. DE algorithm is based on two parameters: the mutation factor and the crossover probability. The fundamental idea behind DE is the use of vector differences by choosing randomly selected vectors and then taking their difference as a means to reach the next vectors.

## 2. Modeling and dimensioning of flat slabs

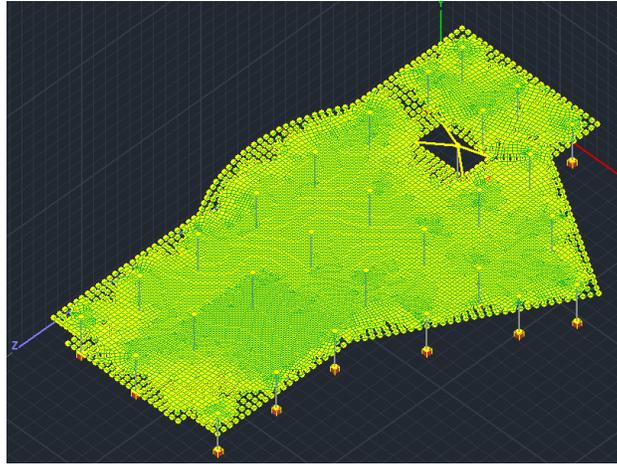


The new version of SCADA Pro offers the possibility of creating flat slabs (slabs without the presence of beams) with the finite element method.

The procedure for the modeling of flat slabs requires:

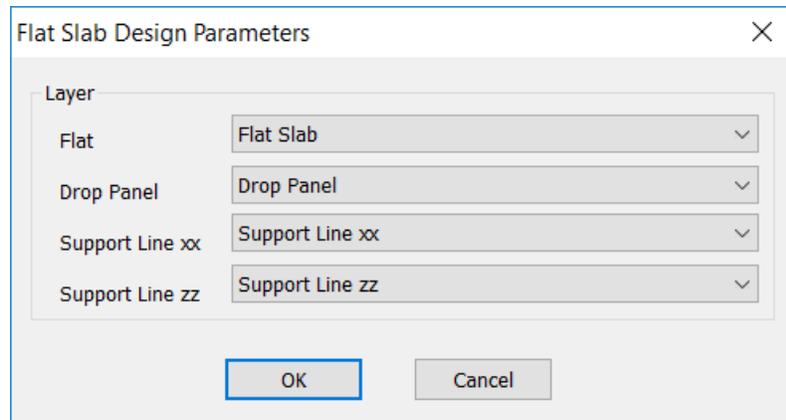
- the 3D Mesh definition,
- the External Boundary creation ,

- the Holes automatically creation in place of the Columns,
- the Mesh calculation and the mathematical model calculation.



The command "Flat slabs" includes the commands:

❖ Parameters



In the dialog box you define the correlation between Layers.

❖ Calculation of design strips

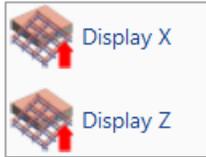


According to Annex I of EC2 flat slab is divided into design strips. These are the areas that are automatically created by the program on both sides of the Support Line, according to Figure I.1 of EC2.

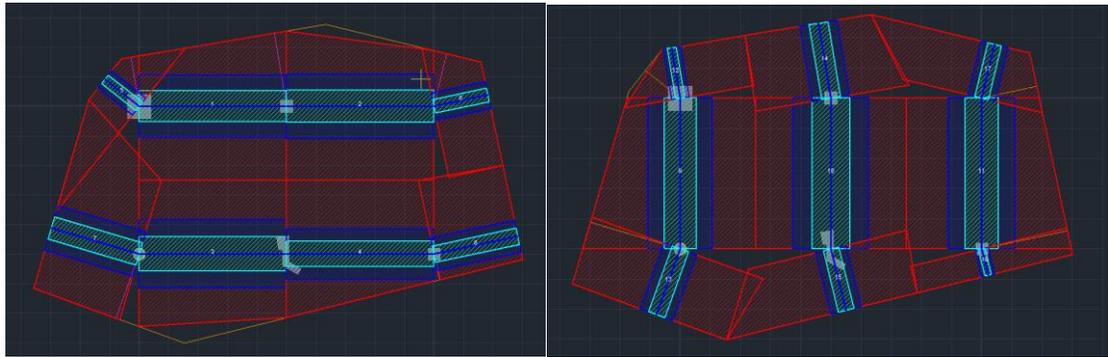
Select the command **Calculation of design strips** and the program automatically creates them.

Each **Design Strip** is divided into sections along its length perpendicular to the **Support Line**. In each section Scada integrates the internal forces of finite surface elements intersect. By completing this occur the bending moment around the axis of the section. This intensive value used to calculate the armature in each section.

❖ **Display X, Z**



Select to display the Design Strips in both directions.

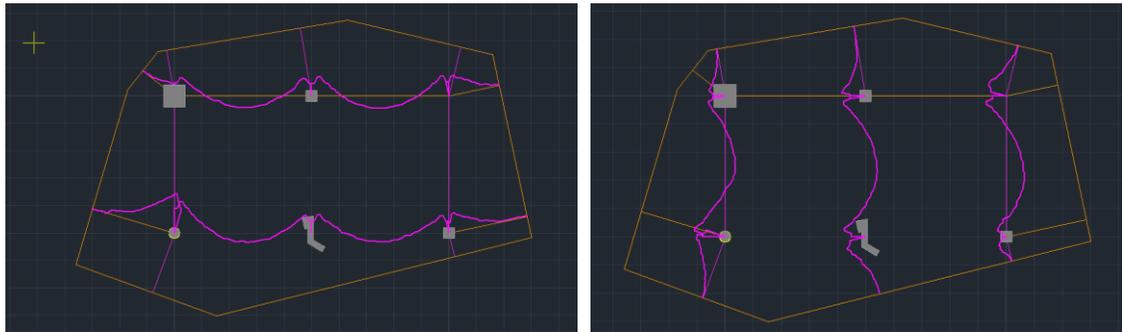


Design Strips along the X and Z axes

❖ **Diagrams X, Z**



Select Diagrams in both directions to see the corresponding diagrams.



❖ Results



This command opens the Results file through the Report.

Each page concerns a Strip Line.

Initially described the characteristics of the Strip.

Strip Calculations							Page : 1
Description	Value	Units	Code	Description	Value	Units	Code
Floor	1			Starting point	corner column		9.4.1&2
# of strip	1			Drop panel	Yes		
Orientation	x-x			Thickness	182.88	(cm)	
Length	815.48	(cm)		Width		(cm)	
Concrete	C20/25			Finishing point	internal column		9.4.1&2
$\epsilon_k$	20	(MPa)	Table 3.1	Drop panel	Yes		
$\epsilon_{cm}$	2.20	(MPa)	Table 3.1	Thickness	182.88	(cm)	
Steel	S400s			Width		(cm)	
$f_{yk}$	400	(MPa)		Minimum reinforcement	0.00143	(cm <sup>2</sup> /m)	
Cover	20	(mm)		Tension reinf.			9.2.1.1(1)
Slab thickness	0.25	(cm)		Compression reinf. (% of span reinf.)	25	%	9.3.1.2

Then displayed the reinforcement results above and below in detail for each zone, dividing them into sub-zones.

Analysis Results and Reinforcement										Top
125.00 cm (L <sub>Left</sub> )					250.00 cm (L <sub>Centre</sub> )					
Zone	M (kNm)	Width (cm)	A <sub>s,req</sub> (cm <sup>2</sup> /m)	A <sub>s,prov</sub> (cm <sup>2</sup> /m)	Φ/s	M (kNm)	Width (cm)	A <sub>s,req</sub> (cm <sup>2</sup> /m)	A <sub>s,prov</sub> (cm <sup>2</sup> /m)	Φ/s
Left	-33.909	86.5	5.660	5.660	8/8		127.5		1.415	8/20
L-C	-45.708	52.7	9.744	9.744	8/5		52.7		2.606	8/19
Center	-170.151	105.3	19.129	19.129	12/5		105.3		4.782	8/10
R-C	-44.750	52.7	9.530	9.530	8/5		52.7		2.382	8/20
Right	-72.082	144.7	5.478	5.478	8/9		144.7		1.369	8/20
125.00 cm (L <sub>Left</sub> )										
Zone	M (kNm)	Width (cm)	A <sub>s,req</sub> (cm <sup>2</sup> /m)	A <sub>s,prov</sub> (cm <sup>2</sup> /m)	Φ/s					
Left	-44.707	149.7	3.284	3.904	8/12					
L-C	-48.725	52.7	10.423	10.423	10/7					
Center	-162.632	105.3	18.175	18.175	12/6					
R-C	-42.495	52.7	9.027	9.027	8/5					
Right	-43.124	144.7	3.240	3.904	8/12					
Analysis Results and Reinforcement										Bottom
125.00 cm (L <sub>Left</sub> )					250.00 cm (L <sub>Centre</sub> )					
Zone	M (kNm)	Width (cm)	A <sub>s,req</sub> (cm <sup>2</sup> /m)	A <sub>s,prov</sub> (cm <sup>2</sup> /m)	Φ/s	M (kNm)	Width (cm)	A <sub>s,req</sub> (cm <sup>2</sup> /m)	A <sub>s,prov</sub> (cm <sup>2</sup> /m)	Φ/s
Left	11.110	86.5	1.380	1.380	8/20	52.042	127.5	5.346	5.346	8/9
L-C	2.346	52.7	0.475	1.438	8/20	27.508	52.7	5.752	5.752	8/8
Center	9.371	105.3	0.952	1.438	8/20	55.015	105.3	5.752	5.752	8/8
R-C	2.362	52.7	0.478	1.438	8/20	27.508	52.7	5.752	5.752	8/8
Right		144.7		0.999	8/20	52.965	144.7	3.995	3.995	8/12
125.00 cm (L <sub>Left</sub> )										
Zone	M (kNm)	Width (cm)	A <sub>s,req</sub> (cm <sup>2</sup> /m)	A <sub>s,prov</sub> (cm <sup>2</sup> /m)	Φ/s					
Left		149.7		1.337	8/20					
L-C		52.7		1.438	8/20					
Center	7.314	105.3	0.742	1.438	8/20					
R-C	8.729	52.7	1.786	1.786	8/20					
Right	27.511	144.7	2.052	2.052	8/20					

### 3. Punching shear checks

Added in the new version also the punching checks in accordance with EC2. The check is part of the check and design process of the flat slabs which runs automatically, but can also run as an individual check for any column. All data can be set automatically or even manually.

**Punching Shear Check** [X]

Control node: 40

Combinations: Combinations  $\Delta N(kN)$  240.82;  $\Delta M_y(kNm)$  8.4002;  $\Delta M_z(kNm)$  31.888; Distributed Load.(kN/m<sup>2</sup>) 0

Materials (MPa): Automatic fck 20 fyk 400

Outlines of floors: Lines circles

Loaded surface: Automatic c1(cm) 46 c2(cm) 46.00; Position of loaded surface: Automatic ax 0 ay 0

Slab's elements: Thickn Automatic t(cm) 25.4; Cover Automatic upper(cr) 2 bottom(cr) 2

Steel Reinforcements: Automatic External X Y; Above  $\Phi$  10 / 15  $\Phi$  10 / 15; Below  $\Phi$  10 / 15  $\Phi$  10 / 15

Coefficient  $\beta$ : Automatic appro:  $\beta$  1.15

Reinforcement Type: Radial; Number of radii per quartile 0

Buttons: Calculation, Results, OK, Deletion of the Report, Cancel

- Production of complete results print out, with detailed reinforcement layout plan (radial or cross), whenever required.
- Details designing.

Page : 1

Input Data					
Description	Value	Units	Description	Value	Units
Level - Storey	1		Eccentric factor ( $\beta$ ) (EC2-6.4.3)	1.150	(cm)
# of node	39		Slab depth	40.6	(cm)
Combination	1		Cover of reinforcement	2.0	(cm)
Shear force ( $V_{Ed}$ )	846.7	(kN)	Bar size (outer layer)	10	(mm)
Distributed load (p)	0.0	(kN/m <sup>2</sup> )	Spacing of bars (outer layer)	15.0	(cm)
Reduced shear force ( $V_{Ed,red}$ )	846.7	(kN)	Bar size (second layer)	10	(mm)
Bending moment ( $M_u$ )	-32.7	(kNm)	Spacing of bars (second layer)	15.0	(cm)
Bending moment ( $M_u$ )	104.4	(kNm)	Concrete ( $f_{ck}$ )	20.0	(MPa)
Shape of loaded area	Rectangular		Steel ( $f_{yk}$ )	400.0	(MPa)
$c_x$ length (along x axis)	45.0	(cm)	Reinforcement pattern	Radial	
$c_y$ length (along y axis)	45.0	(cm)	# of radii of reinforcement in a quadrant (circular pattern)	2	
c diameter	(cm)				
Position of loaded area	Interior				
Dist. of slab perim. along x ( $s_x$ )	(cm)				
Dist. of slab perim. along y ( $s_y$ )	(cm)				

Page : 2

Check results						
Description	Value	Units	EC2	Description	Value	Units
Effective depth of slab (d)	37.6	(cm)	(eq6.32)	Basic control perimeter ( $u_0$ )	657.0	(cm) (fig.6.15)
Perimeter of the loaded area ( $u_1$ )	184.0	(cm)	(eq6.53)	Design value of the shear stress at $u_0$ ( $v_{Ed,0}$ )	0.394	(MPa) (eq6.38)
Design value of the shear stress at $u_0$ ( $v_{Ed,0}$ )	1.406	(MPa)	(eq6.38)	Punch. shear resistance without shear reinforcement ( $V_{Rd,c}$ )	0.356	(MPa) (eq6.47)
Maximum punching shear resistance ( $V_{Rd,max}$ )	3.660	(MPa)	(eq6.53)	Constant ( $v_{Rd,c}$ )	0.356	(MPa) (eq6.3)
1 <sup>st</sup> check: $v_{Ed,0} \leq V_{Rd,max}$	Sufficiency			2 <sup>nd</sup> check: $v_{Ed,1} \leq V_{Rd,c}$		
				Reinforcement necessary: - add punching shear reinforcement - increase slab longitudinal reinforcement		

Detailing results						
Description	Value	Units	EC2	Typ/prop	Min/Max	EC2
Perimeter $u_{load}$	727.0	(cm)	(eq6.54)	Distance ( $d_1$ )		(cm)
(a) - Distance of 1 <sup>st</sup> perimeter of reinforcement from the loaded area	18.8	(cm)		Angle ( $\varphi$ )	90.0	°
Limit: $0.3 \cdot d \leq a \leq 0.5 \cdot d$	11.3 < 18.8 < 18.8	(cm)	(9.4.3)	( $s_{u,0}$ ) - Tangential distance between link legs on the last perimeter	91.8	(cm)
(f) - Distance of last perimeter of reinforcement from $u_{load}$	56.6	(cm)		Limit 2.0 d	75.3	(cm)
Limit: $k \cdot d = 1.5 \cdot d$	56.5	(cm)	(6.4.5)	( $s_{u,1}$ ) - Effective design strength of punching shear reinf.	344.1	(MPa) (eq6.52)
(s <sub>1</sub> ) - Radial distance of the perimeters of reinforcement	28.0	(cm)		( $A_{s,u,1}$ ) - Necessary area of a link leg	1.532	(cm <sup>2</sup> )
Limit: 0.75 d	28.2	(cm)	(9.4.3)	( $A_{s,u,2}$ ) - Minimum area of a link leg	1.532	(cm <sup>2</sup> ) (eq9.11)
(s <sub>2</sub> ) - Tangential distance between link legs on the $u_1$ perimeter	91.8	(cm)		Limit: 1.5 d	56.5	(cm) (9.4.3)
Limit: 1.5 d	56.5	(cm)	(9.4.3)	Distance (p)	18.1	(cm)
Distance (p)	18.1	(cm)		Distance (d <sub>1</sub> )	9.9	(cm)
Distance (d <sub>1</sub> )	9.9	(cm)		Distance (d <sub>2</sub> )	9.9	(cm)

Grouping of punching shear reinforcement						
Group	Number of lines	$\phi$ (mm)	Number of link legs on line	Height of link leg (cm)	Perimeter where the 1 <sup>st</sup> link leg of the line stands	Distance of the 1 <sup>st</sup> link leg from the loaded area
1	8	14	2	36.6	1	16.82
2	4	14	1	36.6	2	46.82